

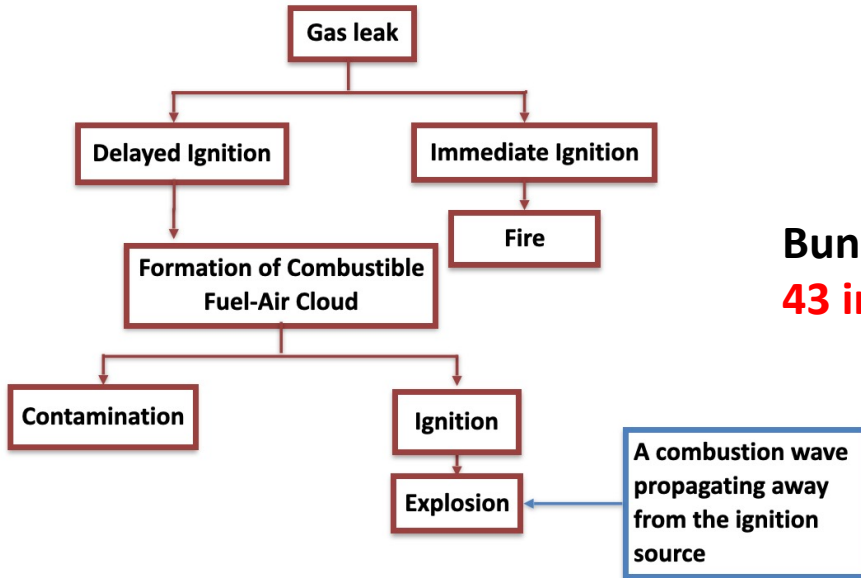
From Deflagration to Detonation



O. Dounia, CERFACS

Explosion events, tragic scenarios

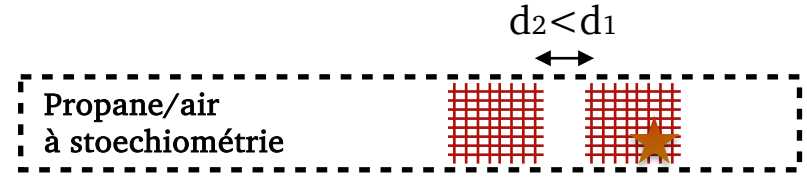
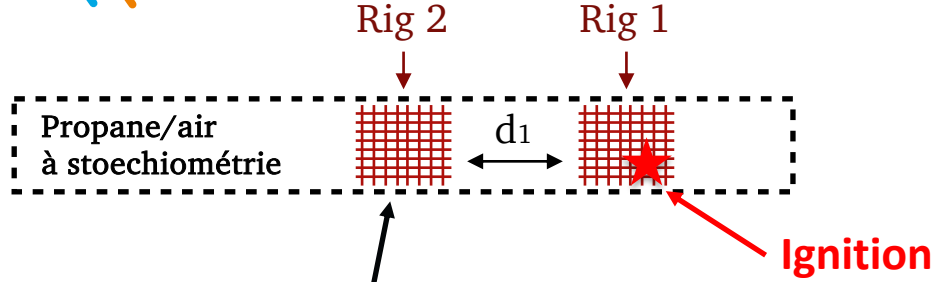
Taijin, 2015
173 fatalities,
43 injuries



Buncefield, 2005
43 injuries



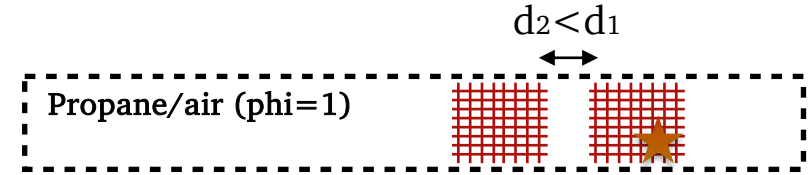
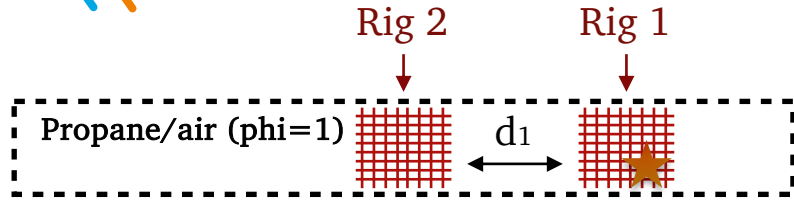
2 regimes of explosions



JIP MEASURE [1]

[1] Masri et al., IECR 2012

2 regimes of explosions



Deflagration to Detonation Transition (DDT)



Deflagration scenario



- Small changes in setup => **extreme escalation of the explosion scenario**
- Could suggest a change in “combustion regime”
 - Safety : Necessity to understand the triggering mechanisms of this transition

■ ■ ■ ■ ■ ■ [1] Masri et al., IECR 2012



Specificities of H2

- Safety : Necessity to understand the triggering mechanisms of DDT
- True for any fuel ...
 - ... **BUT particularly true for H2**
 - H2 has some specificities that challenge many safety strategies**
 - High tendency to: leak, ignite and “detonate”**

Properties		Hydrogen	Methane	Gasoline
Minimum ignition energy in air (MIE)	(mJ)	0,02	0,29	0,24
Flammability limits in air	(vol. %)	4 - 75	5,3 - 15	1,0 - 7,6
Detonation limits in air	(Vol. %)	13 - 65	6,3 - 13,5	1,1 - 3,3 [1,2]

Accidentology involving hydrogen, BARPI report, 2007
A.E. Dahoe, JLPPI 2005

Disclaimer



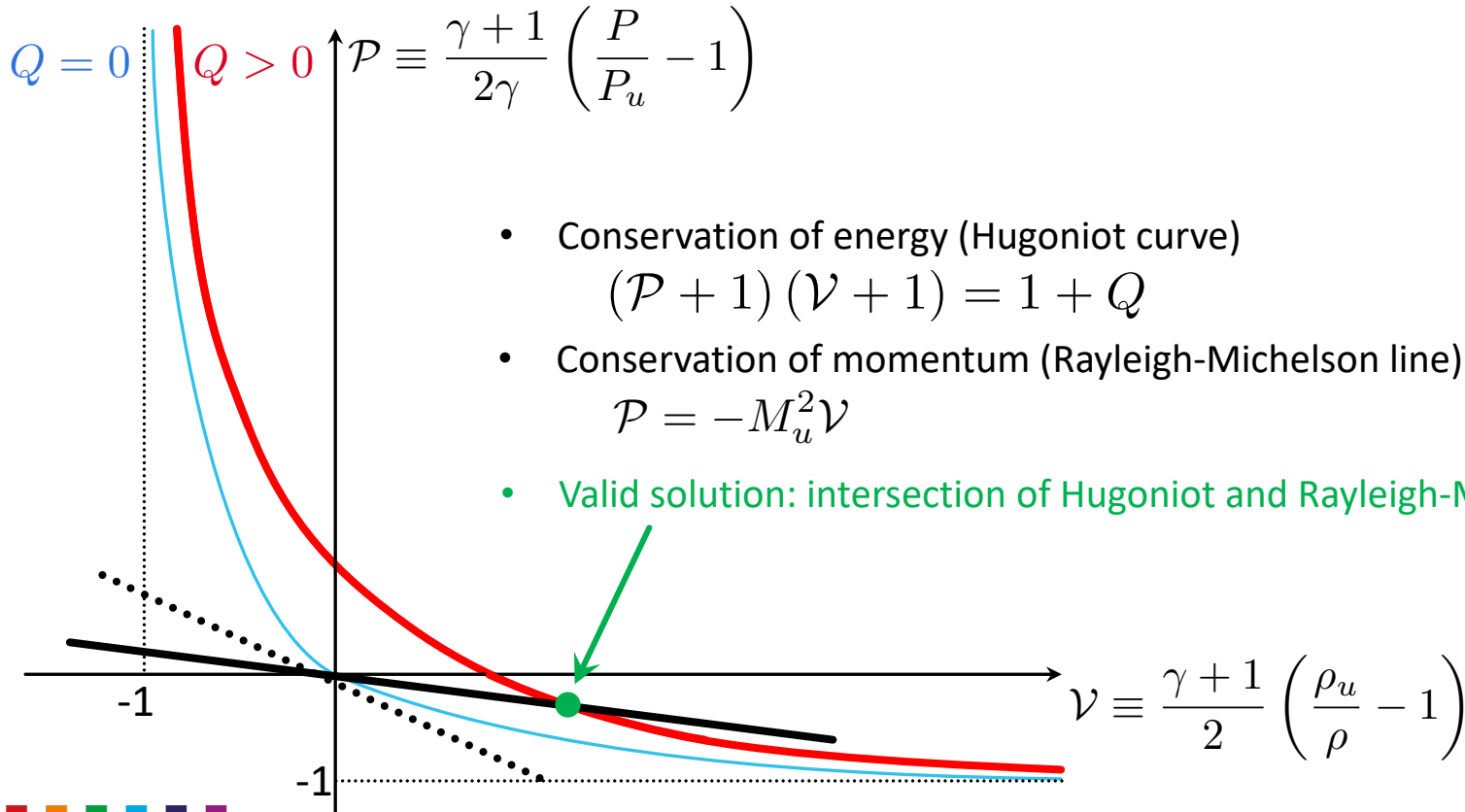
- We assume the conditions for direct detonation initiation are not met
 - i.e. the scenario never starts with the violent regime of explosion
 - Requirements too strong (strong blast decay):
 - $E_c \geq 10^4$ (H_2); 10^5 (C_2H_4); 10^6 (C_3H_8) [J] [1]
 - Consistent with observations from industrial accidents



Existence of two regimes of combustion: Based on conservation laws

Generalized Rankine-Hugoniot relations

- Set of thermodynamic relations that planar exothermic waves must satisfy

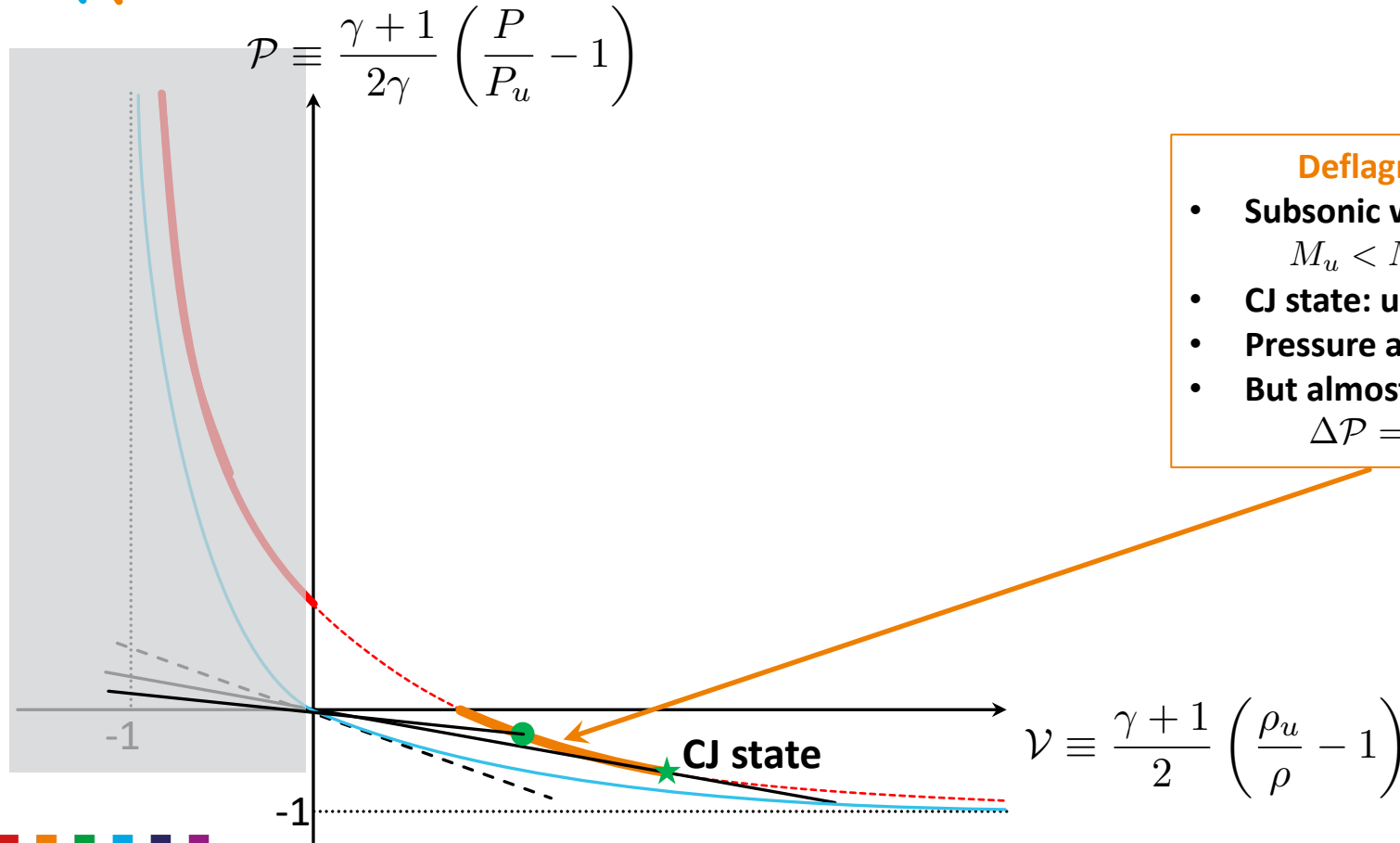


$D = \text{cst}$
 Burnt Unburnt

$$Q \equiv \frac{\gamma + 1}{2} \left(\frac{q_m}{c_p T_u} \right)$$

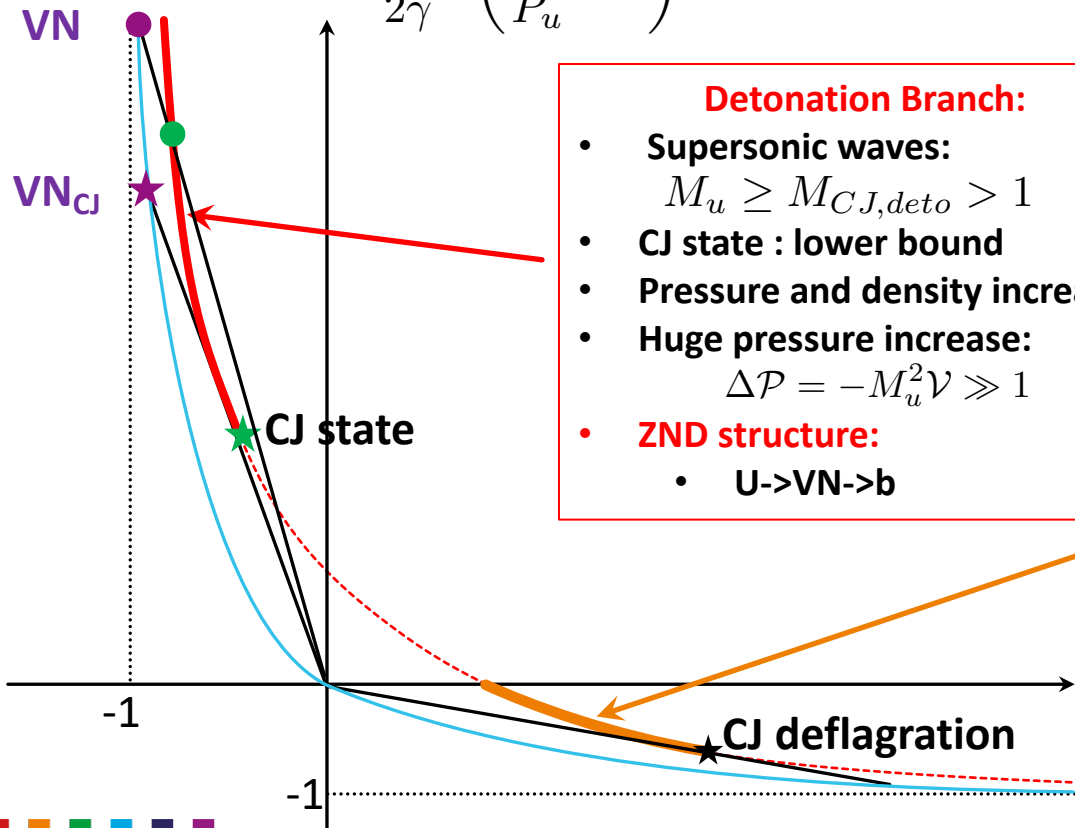
$$M_u = \frac{D}{a_u}$$

The deflagration branch



The detonation branch

$$\mathcal{P} \equiv \frac{\gamma + 1}{2\gamma} \left(\frac{P}{P_u} - 1 \right)$$



Detonation Branch:

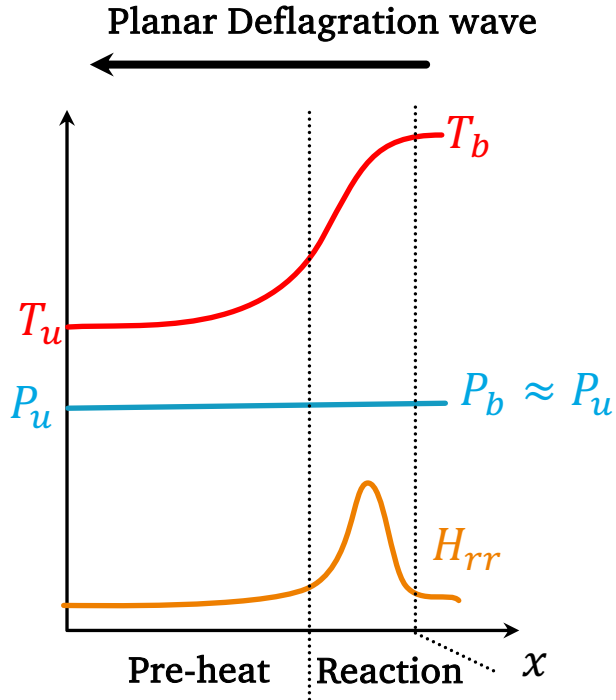
- **Supersonic waves:**
 $M_u \geq M_{CJ,deto} > 1$
- **CJ state : lower bound**
- **Pressure and density increase**
- **Huge pressure increase:**
 $\Delta P = -M_u^2 \mathcal{V} \gg 1$
- **ZND structure:**
 - U->VN->b

Deflagration Branch:

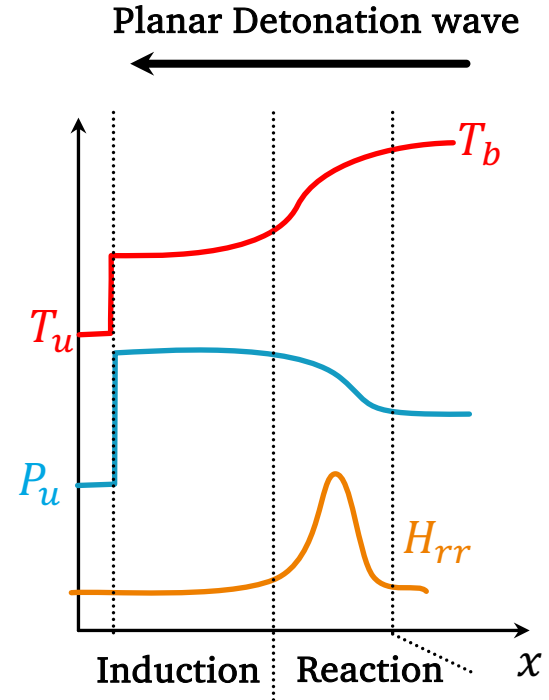
- **Subsonic waves:**
 $M_u < M_{CJ,deflag} \ll 1$
- **CJ state: upper bound**
- **Pressure and density decrease**
- **But almost isobaric:**
 $\Delta P = -M_u^2 \mathcal{V} \ll 1$

$$\mathcal{V} \equiv \frac{\gamma + 1}{2} \left(\frac{\rho_u}{\rho} - 1 \right)$$

Internal structure of deflagration and detonation waves

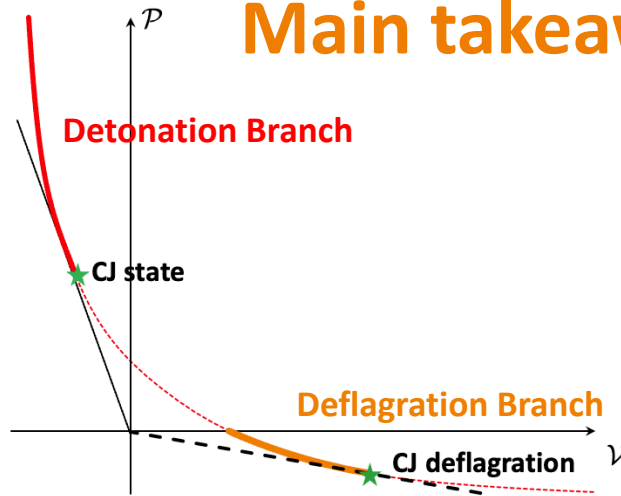


Propagation by diffusion



Propagation by reaction-assisted shock

Main takeaway



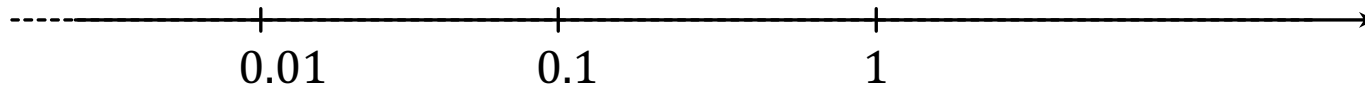
Deflagration Branch:

- Relatively slow,
 $M_u \leq 10^{-2}$
- Almost isobaric
 $P \approx cst$ ⚠

Detonation Branch:

- Supersonic
 $M_u \geq 4 - 5$
- Huge pressure increase:
 $P_b > 10P_u$; $P_{VN} > 20P_u$

Gap in acceptable solutions



$$M_u = \frac{D}{a_u}$$



Relative velocities

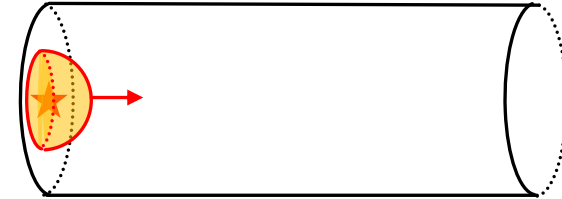
- Conservation laws predict a huge gap in acceptable solutions
- A naïve conclusion:
“If my scenario starts with a deflagration, I am safe”



DDT in lab-scale experiments: Observations

Experimental observations

- Typical experiment:
 - Closed tube or channel filled with reactive mixture (obstacles optional)
 - Ignite on one end
 - Flame kernel formation and propagation in the mixture



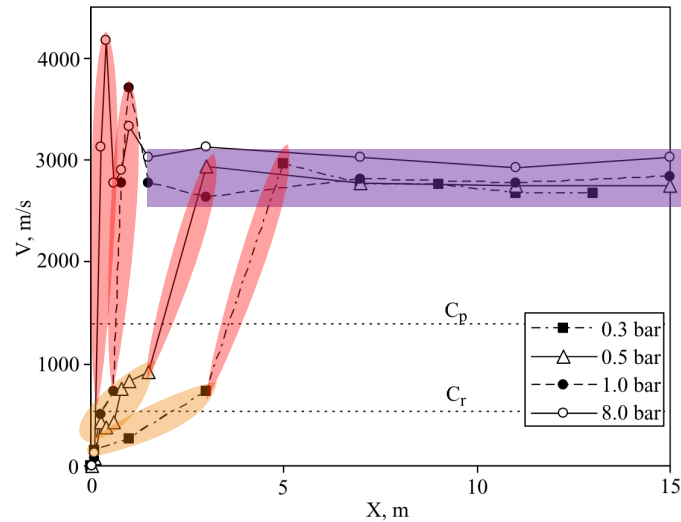
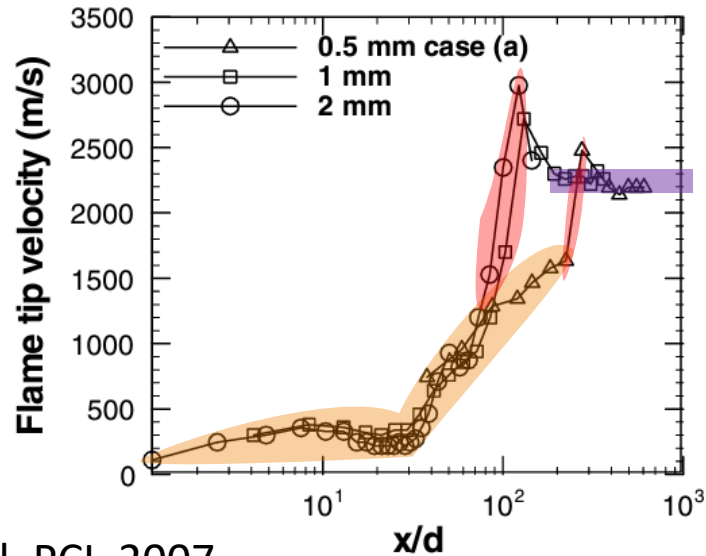
Objective:

Evolution of the **self-propagating** flame inside the tube/channel

Key variable: **flame propagation velocity** (laboratory frame of reference)

3 phases of DDT scenarios

- 1) Flame acceleration (FA) : precursor of DDT
- 2) Sudden acceleration: DDT
- 3) Detonation propagation: Relax to a C_{st} speed (when possible)
 - Remarkably close to the Generalized Rankine-Hugoniot



Wu et al, PCI, 2007

Kuznetsov et al, Shock Waves, 2005



- 1) Flame acceleration (FA) : precursor of DDT
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A recipe for strong FA

- Flames are intrinsically unstable reaction waves
- Many mechanisms can accelerate a flame front (coupling possible)
- The following is a recipe for a very efficient FA

WARNING
Safety engineer discretion is advised

First FA following ignition

Recipe for a strong FA:

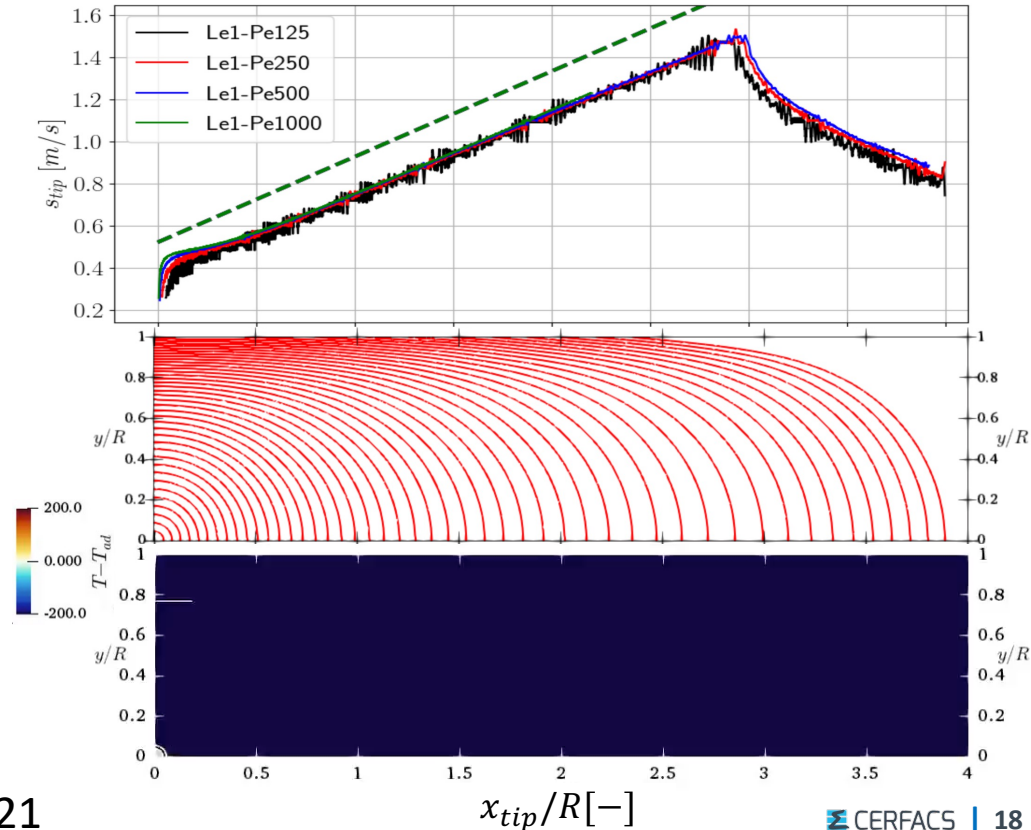
1) 1 table spoon of confinement

- Finger-shaped flame
- FA Exponential in time

$$\frac{dX_{tip}}{dt} = \sigma s_L^0 + (\sigma - 1) s_L^0 (X_{tip}/R) \quad \sigma \equiv \rho_u / \rho_b$$

- BUT limited in time

H₂/air, $\phi = 0.36$, $P = 1 \text{ atm}$, $T_u = 300 \text{ K}$, $Le_{eff} = 1$ [1]

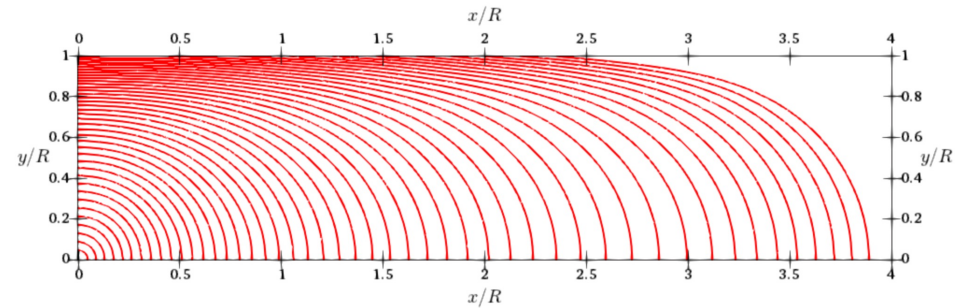
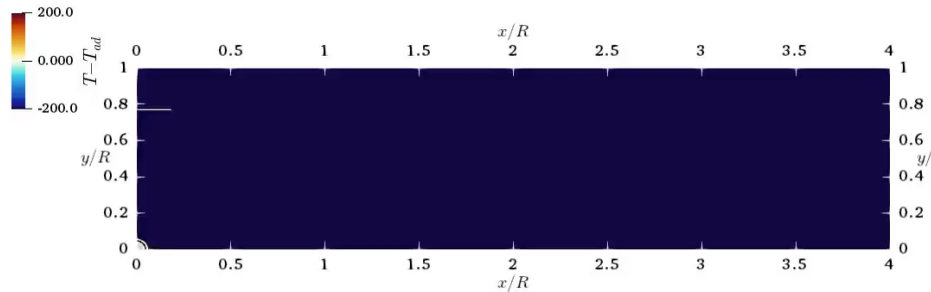


[1] J. J. Hok, et al., ICDERS 2021

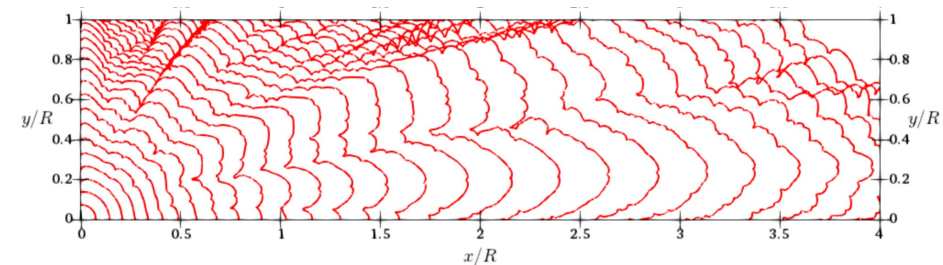
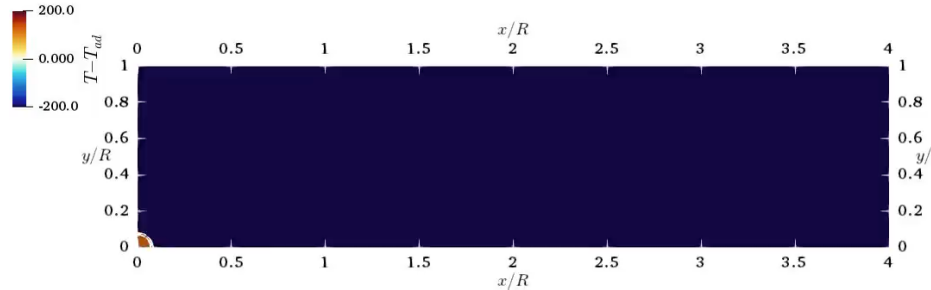


Flame instabilities

Typical finger flame acceleration: H2/air, $\phi = 0.36, P = 1\text{atm}, T_u = 300\text{K}, Le_{eff} = 1$ [1]

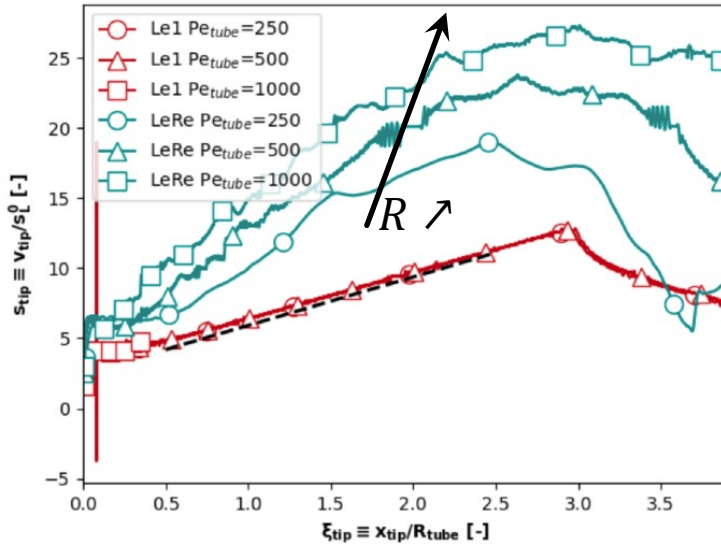


Thermo-diffusively unstable flames: H2/air, $\phi = 0.36, P = 1\text{atm}, T_u = 300\text{K}, Le_{eff} = 0.3$ [1]

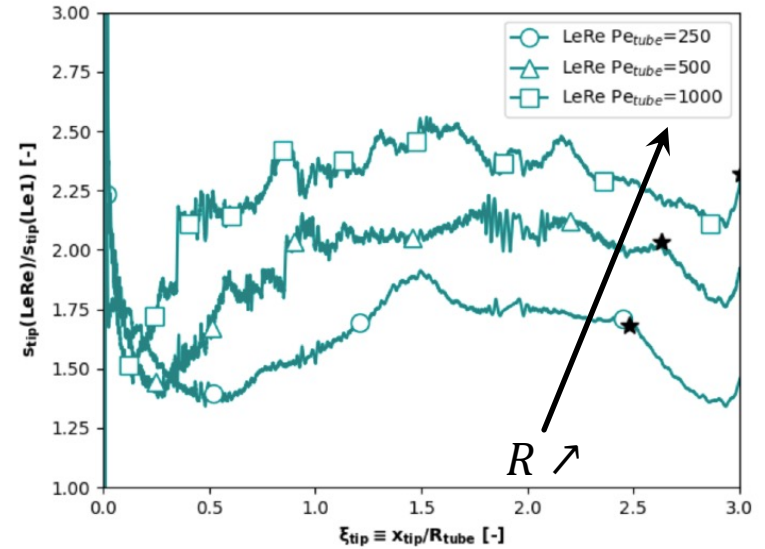


Early stages of flame acceleration

Coupling between thermo-diffusive effects and geometrical acceleration



Additional contribution of TD
Depends on confinement (R)



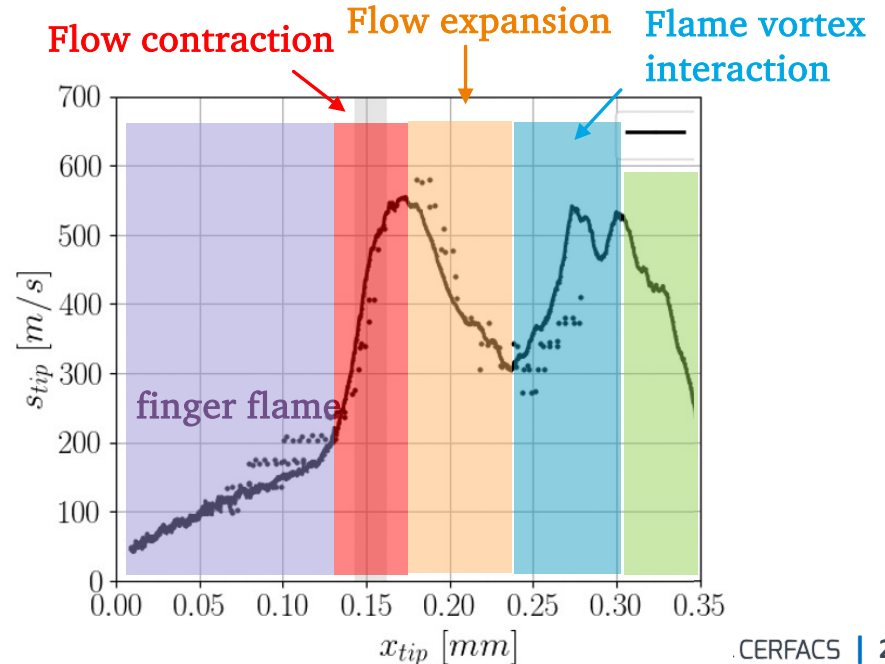
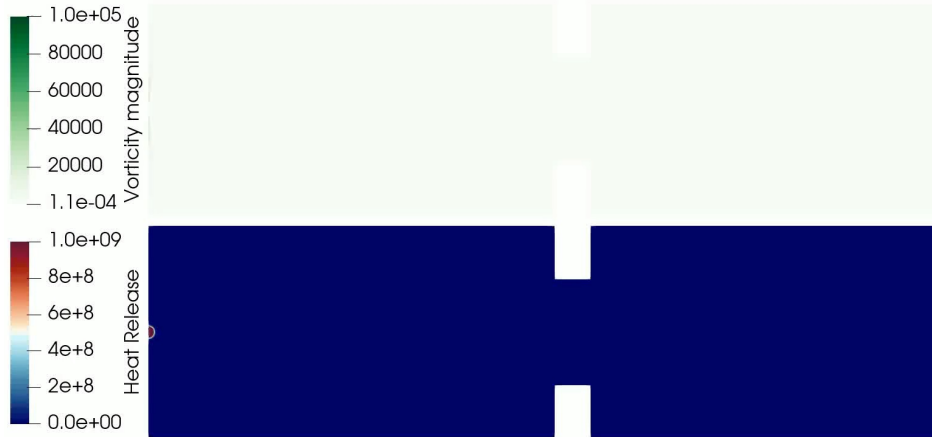
Going beyond the early stages: obstacles

Recipe for a strong FA:

- 1) 1 table spoon of confinement
- 2) **1 pinch of obstruction**

- Flame=semi-permeable piston (sets reactivities in motion)
- Flame/obstacle interaction: strong FA
 - Depends on obstacle configuration (shape, BR)
- BUT also limited to the vicinity of the obstacle

$H_2/O_2, \phi = 1., P = 15kPa, T_u = 300K$ [1]



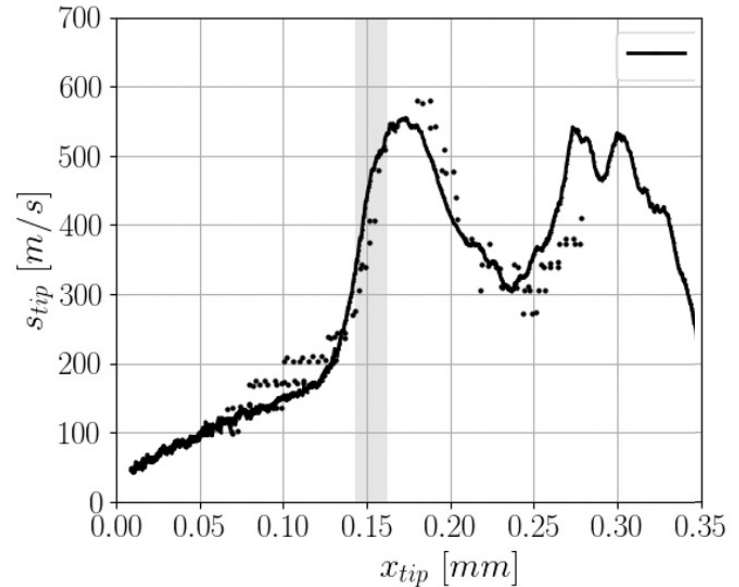
Going beyond the early stages: obstacles



s_{tip}

- Absolute speed on an iso-level surface
- Includes both burning and advection by the flow
- Not a burning velocity relative to fresh gases

The reaction wave is still subsonic relative to fresh gases
(deflagration branch)





The remarkable efficiency of repeated obstacles

Recipe for a strong FA:

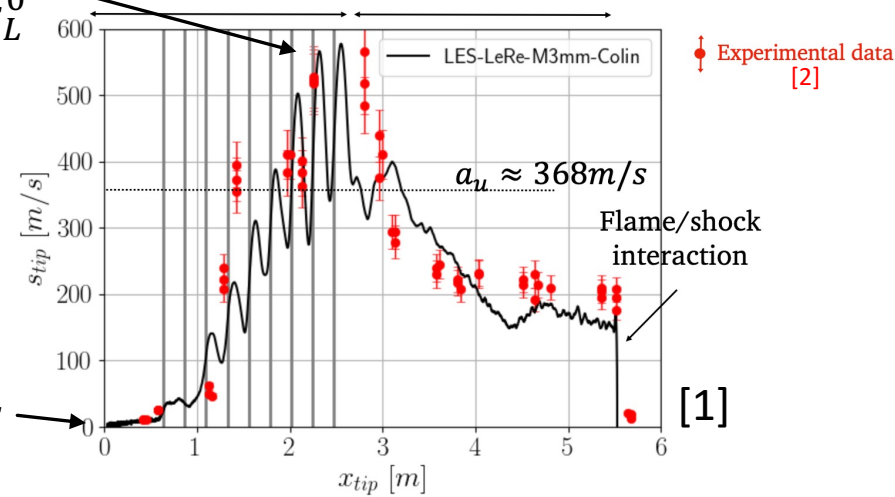
- 1) 1 table spoon of confinement
- 2) 1 pinch of obstruction
- 3) 1 gallon of obstruction

$$s_{tip} \approx 600 \text{ m/s}$$

$$\approx 1000 \sigma s_L^0$$

Obstructed Region: Gradual FA

Free Region: Gradual deceleration



Experimental data [2]

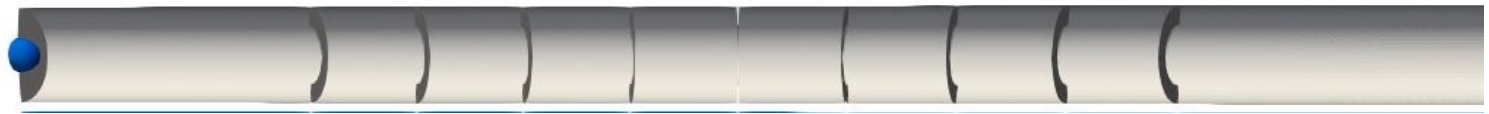
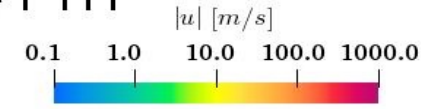
[1]

Strong sensitivity to obstacle configuration: spacing and BR

$$\sigma s_L^0 \approx 0.6 \text{ m/s}$$

Time : 1.00 ms

Flame position: 0.041 m



[1] J. J. Hok, PhD 2024

[2] R. Gorseuvres, PhD 2018



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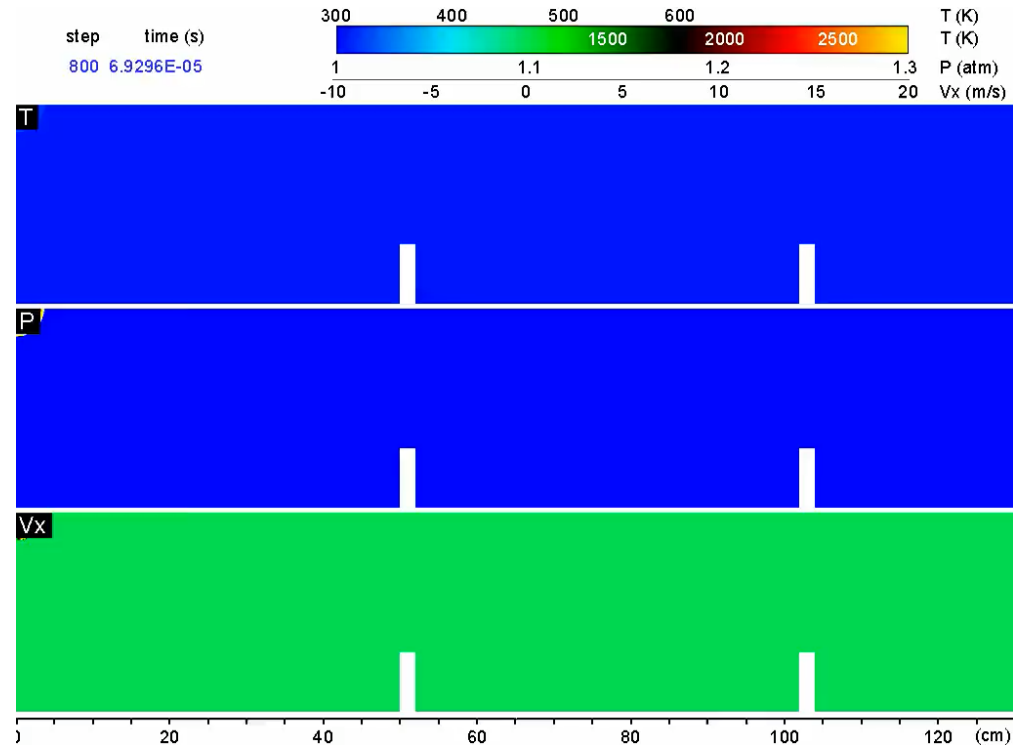
Two classes of DDT mechanisms

- Many mechanisms to explain DDT
- Overall, 2 classes to be distinguished:

1) DDT involving shock waves

- Localised thermal explosion [1]
(Zeldovich or SWACER mechanism)
- Require a strong FA
- Compressibility and shock formation
- Bring the mixture to ignitable conditions (not a sufficient condition!!!)

Courtesy of Pr. E. Oran



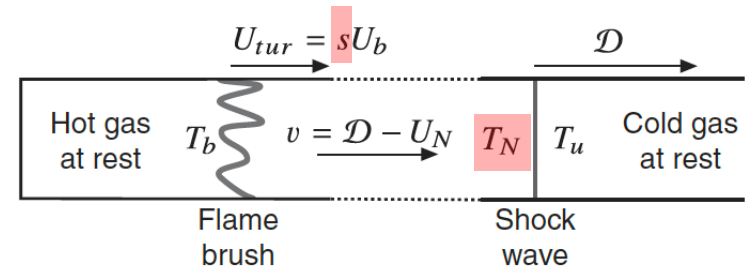
[1] A. Oppenheim and R. Soloukhin, Ann. Rev FM, 1973

Two classes of DDT mechanisms

- Many mechanisms to explain DDT
- Overall, 2 classes to be distinguished:

1) DDT involving shock waves

- Localised thermal explosion[1] (Zeldovich or SWACER mechanism)
- Thermal runaway [2,3]
 - Thermal sensitivity of the flame speed
$$U_b = f(T_N)$$
 - Critical degree of flame folding s^*
 - No self-similar solution above s^*



[1] A. Oppenheim and R. Soloukhin, Ann. Rev FM, 1973

[3] L. Kagan and G. Sivashinsky, PCI, 2014

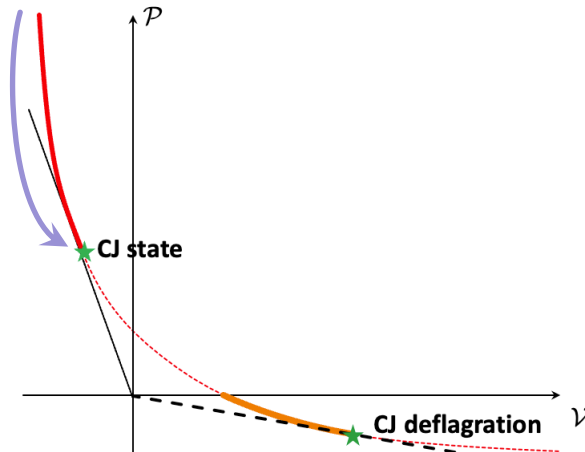
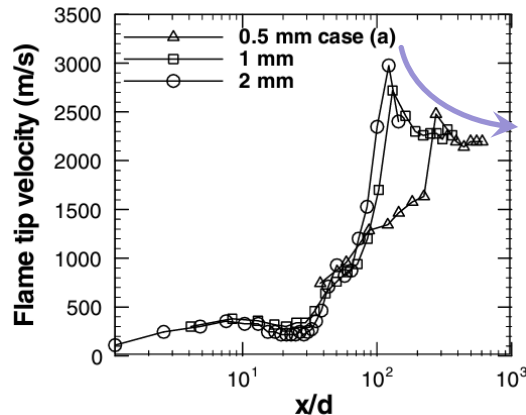
[2] B. Deshaies and G. Joulin, C&F, 1989



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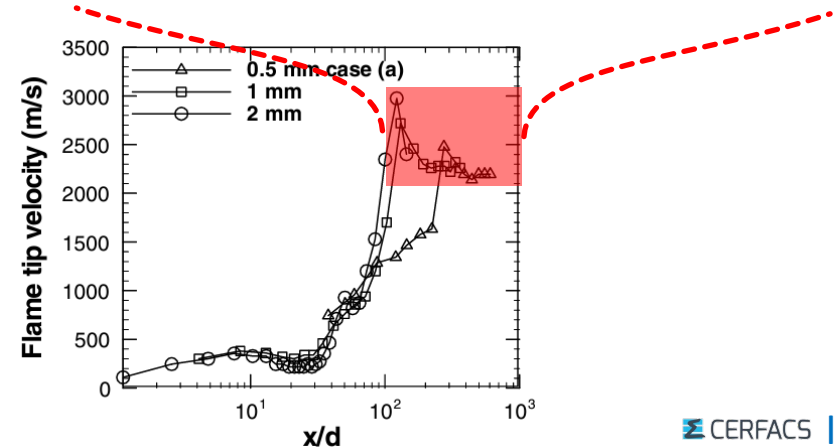
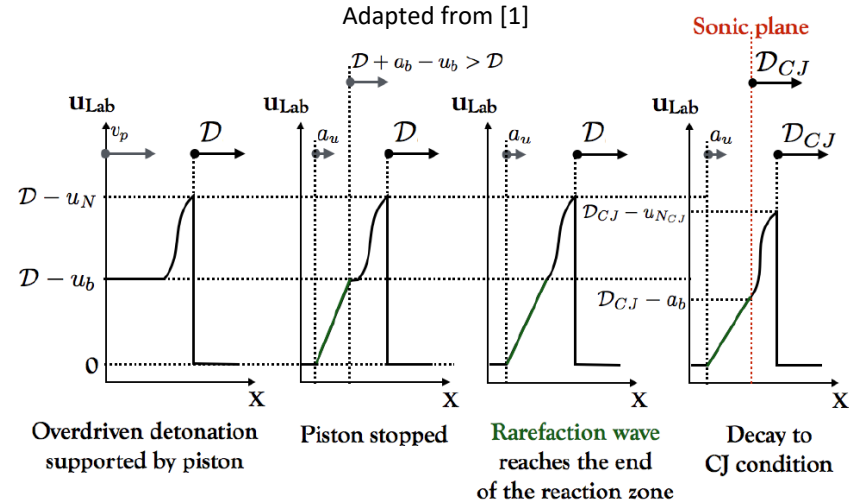
The specificity of the CJ detonation

- Experimental observation:
 - A decay to CJ detonation is often observed
 - Existence of a selection mechanism once detonations are formed
- The key point: the burnt gas state
 - Overdriven detonations: the flow post-reaction is subsonic (reference frame of the detonation)
 - CJ detonation: the flow post-reaction is **sonic**



Relax to CJ

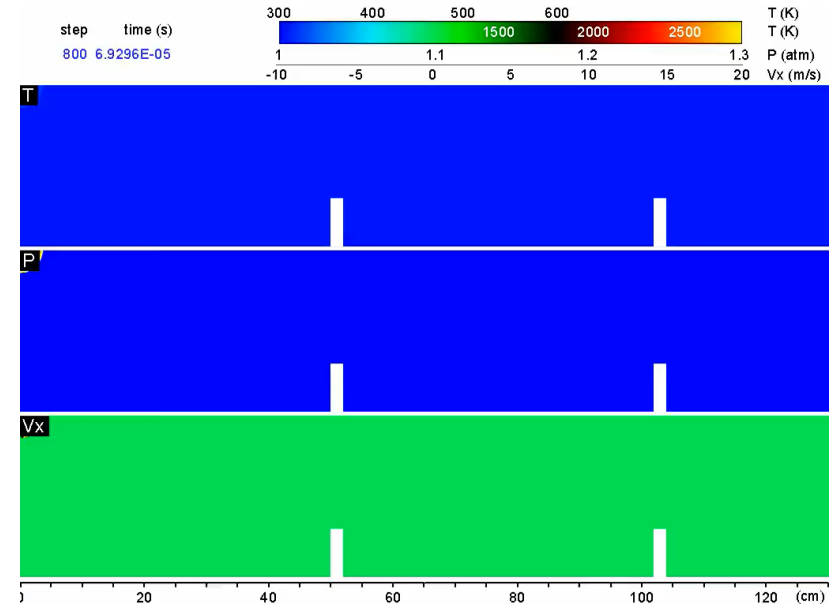
- Overdriven detonations are unstable and can not self-propagate
- Overdriven detonations exist only when supported by a piston (local explosion)
- As soon as the piston support stops:
 - Decay to CJ
 - At CJ: detonation wave protected by the sonic plane
 - CJ solution is the only solution allowing autonomous detonation waves



[1] P. Clavin and G. Searby, Cambridge University Press, 2016

Concluding remarks

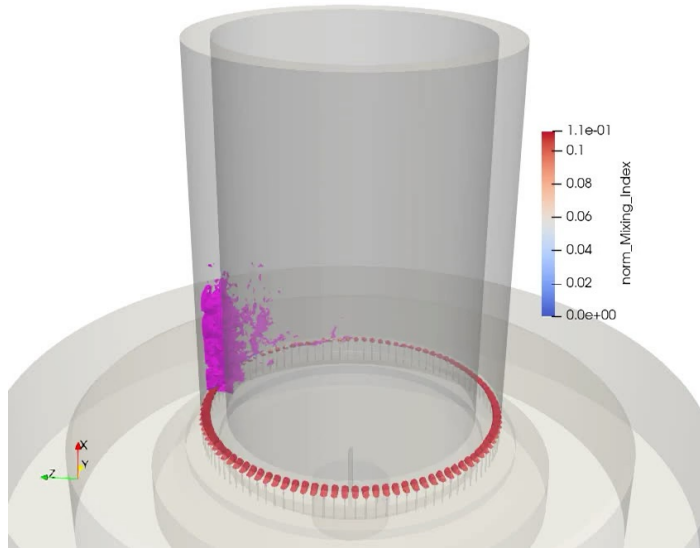
- No universal mechanism behind FA/DDT
- Often, combination of different mechanisms can explain FA/DDT
- Most experiments (even when well-instrumented) do not provide the details behind DDT
- High-fidelity simulations of FA/DDT at scales of industrial relevance is still a difficult task
 - the large range of scales at play
 - Constantly evolving



Detonations can also be useful

RDE simulation

P. Stempf, PhD, 2024



RDE start-up

Credit: James Koch/University of Washington

