

ASME Turbo-Expo, Vancouver, Canada, June 6-10, 2011

# Panel Session 4-34 - LES Modeling of Combustors:

# **CERFACS Perspective**

L.Y.M. Gicquel<sup>1</sup> B. Cuenot<sup>1</sup>, G. Staffelbach<sup>1</sup>, O. Vermorel<sup>1</sup>, E. Riber<sup>1</sup>, A. Dauptain<sup>1</sup> T. Poinsot<sup>2</sup>

> <sup>1</sup> CERFACS - CFD Team, Toulouse <sup>2</sup> IMFT, Toulouse

> > http://www.cerfacs.fr Laurent.Gicquel@cerfacs.fr





CERFACS European Center for Research and Advanced Training in Scientific Computation

#### What's CERFACS?

#### **CERFACS** has seven shareholders

Parallel algorithms

One hundred people in 5 teams



![](_page_2_Picture_0.jpeg)

complex

# CFD research in Turbulent reacting flows has massively transitioned to LES:

- 1996 First TNFS workshop (Naples):
  - => Construct an experimental data base to validate CFD modeling
- 1998 Third TNFS workshop (Bolder):
  - => First comparisons of simple flames expe. / RANS
- 2010 Tenth TNFS workshop (Beijing):

=> Detailed comparisons of expe. / LES

![](_page_2_Picture_9.jpeg)

![](_page_3_Picture_0.jpeg)

# For the specific problem of Gas Turbines

• *Advanced CFD* and *Massively parallel* computer architectures offer a clear potential for time and cost reductions of the design chain while providing *more accurate predictions* 

- CFD modeling needs to be specifically addressed for the three engine components:
  - => Compressor RANS (URANS / LES)
  - => Burner RANS / LES
  - => Turbine RANS (URANS / LES)

• Each component is the locus of distinct flow physics and adding **multi-physics** may greatly contribute to the predictions

- => Flow separation and transition
- => Multi-phase flows
- => Chemical reaction
- => Mixing, cooling
- => Heat transfer

![](_page_3_Picture_14.jpeg)

#### Outline of the talk

![](_page_4_Picture_1.jpeg)

# I] Recent contributions of LES to Combustor design:

- => Real scale applications
  - --> comparison against RANS predictions
  - --> mesh sensitivity analysis
- => Thermo-acoustic instability prediction

# II ] LES perspectives and applications:

- => LES modeling and code validations
- => Transient reacting flows: ignition process understanding

# III ] Perspectives:

=> Towards multi-physics CFD based on LES

# IV ] Conclusions:

L. Gicquel, ASME Turbo-Expo, Vancouver, Canada, June 6-10, 2011

![](_page_4_Picture_14.jpeg)

1.5 2.0 time after t0 [s]

1.0

2.5 3.0x10<sup>-3</sup>

#### Outline of the talk

![](_page_5_Picture_1.jpeg)

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![](_page_5_Picture_14.jpeg)

![](_page_5_Picture_15.jpeg)

![](_page_5_Picture_16.jpeg)

![](_page_6_Picture_0.jpeg)

Target configuration: a helicopter combustion chamber at cruise conditions

![](_page_6_Figure_3.jpeg)

![](_page_7_Picture_0.jpeg)

![](_page_7_Picture_1.jpeg)

#### Target configuration: Single sector gaseous (partially premixed) LES [1]

![](_page_7_Figure_3.jpeg)

![](_page_8_Picture_0.jpeg)

**RANS versus LES :** Impact on a design criterion (i.e. RDTF) [1,2,3]

$$RTDF(r) = \frac{\left\langle \overline{T}(r,\theta) \right\rangle_{\theta} - \left\langle \overline{T}(r,\theta) \right\rangle_{\theta r}}{\left\langle \overline{T}(r,\theta) \right\rangle_{\theta r} - \overline{T}_{inlet}}$$

**Plane of** interest

RTDF(r) profile measures the radial temperature heterogeneities through the exit plane of the chamber  $\Rightarrow$  controls the turbine lifetime !!

![](_page_8_Figure_6.jpeg)

![](_page_8_Picture_7.jpeg)

[3] S. James et al., AIAAJ, 44:674-686, 2007.

![](_page_8_Picture_9.jpeg)

![](_page_9_Picture_0.jpeg)

# Effect of grid resolution: overview for a real combustor application [1,2]

LES in a single sector burner

[1] G. Boudier et al., C&F., 155:196-214, 2008.[2]. G. Boudier et al., QLES, Leuven, 2007.

![](_page_9_Figure_5.jpeg)

![](_page_10_Picture_0.jpeg)

#### I.1 ] Mesh sensitivity analysis

Effect of grid resolution: overview for a real combustor application [1,2]

![](_page_10_Figure_3.jpeg)

![](_page_10_Figure_4.jpeg)

![](_page_11_Picture_0.jpeg)

![](_page_11_Picture_1.jpeg)

# Extending to the full annular burner: thermo acoustic instabilities

#### <u>Numerical aspects:</u>

- ➢ 3D compressible LES (AVBP),
- reactive Navier-Stokes solver,
- ➤ TTGC convective scheme (3<sup>rd</sup> order),
- Smagorinsky model [1],
- NSCBC boundary conditions [2],
- Initial conditions from statistically
  - converged mono-sector results.

![](_page_11_Picture_11.jpeg)

#### What do you get out of the 1,000,000 CPU-hours spent ??

#### <u>Chemical aspects:</u>

- > JP10 1-step fitted mechanism (surrogate for kerosen [3])
- Dynamic Flame Thickening [4].

#### [1] Smagorinsky et al., 1963

[2] Poinsot et al., 1992

[3] Légier et al., 2001

[4] Colin et al., 2000

L. Gicquel, Complex Flows, KAUST, March 22-25, 2010.

![](_page_11_Picture_21.jpeg)

G. Boufier et al., IJ Aeroacoustic, 2007

![](_page_11_Picture_23.jpeg)

![](_page_12_Picture_0.jpeg)

#### I.1 ] Thermo acoustic instability

Application to full annular burner: impact on pressure

![](_page_12_Figure_3.jpeg)

• Temporal evolution of pressure typical of the expression of two counter-rotating pressure waves: self-sustained azimuthal thermo-acoustic instability.

![](_page_12_Picture_5.jpeg)

![](_page_13_Picture_0.jpeg)

![](_page_13_Picture_1.jpeg)

Application to full annular burner: impact on temperature

![](_page_13_Figure_3.jpeg)

the entire engine...

# 38.36000 ms

• Unexpected implication of the instability: azimuthal oscillation of combustion and the temperature field.

![](_page_13_Picture_7.jpeg)

L. Gicquel, Complex Flows, KAUST, March 22-25, 2010.

#### Outline of the talk

![](_page_14_Picture_1.jpeg)

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![](_page_14_Picture_14.jpeg)

1.5 time after t0 [s]

2.0

15

1.0

![](_page_14_Picture_15.jpeg)

![](_page_14_Picture_16.jpeg)

![](_page_14_Picture_17.jpeg)

![](_page_15_Picture_0.jpeg)

# Gaseous turbulent combustion validation:

#### Premixed combustion

PRECCINSTA burner [1,2]: atmospheric rig targeted to understand thermo-acoustic instabilities --> Measured profiles of Velocity (LDV), Species and Temperature fields (Raman) for different operating cdts (i.e. equivalence ratio – stable & unstable combustion)

#### Axial velocity RMS profiles [3-6]:( $\Phi$ =0.8)

![](_page_15_Figure_6.jpeg)

![](_page_16_Picture_0.jpeg)

One difficulty for LES when faced with these setups is to go after more specific quantities: intermediate species of reactions & pollutant formations... <sup>[1]</sup> B. Franzelli et al., C&F, 157:1364-1373, 2010. [2] W.P. Jones et al., C&F 73:222-233, 1988. => what model / chemical scheme to use and how ?? [3] N. Peters, Vol. 241, Springer, Berlin, 1985.

2 step reduced scheme [1]

 $\begin{array}{rcl} {\it CH4} + 1.5 \,\, {\it O}_2 & => & {\it CO} + 2 \,\, {\it H}_2 {\it O} \\ {\it CO} + 0.5 \,\, {\it O}_2 & <=> & {\it CO}_2 \end{array}$ 

![](_page_16_Figure_5.jpeg)

4 step reduced scheme [2]		
$CH_4 + 0.5 O_2$	=>	$CO + 2 H_2$
$CH_4 + H_2O$	=>	$CO + 3 H_2$
$CO + H_2O$	<=>	$CO_2 + H_2$
$H_2 + 0.5 O_2$	<=>	$H_2O$

![](_page_16_Figure_7.jpeg)

#### 4 step reduced scheme [3]

 $\begin{array}{rcl} CH_4 + 2 \ H + \ H_2O & => & CO + 4 \ H_2 \\ CO + \ H_2O & <=> & CO_2 + H_2 \\ 2 \ H + M & <=> & H_2 + M \\ 3 \ H_2 + O_2 & <=> & 2 \ H + 2 \ H_2O \end{array}$ 

![](_page_16_Figure_10.jpeg)

![](_page_17_Picture_0.jpeg)

B. Franzelli et al., C&F, 157:1364-1373, 2010.
 W.P. Jones et al., C&F 73:222-233, 1988.
 N. Peters, Vol. 241, Springer, Berlin, 1985.

![](_page_17_Figure_3.jpeg)

![](_page_18_Picture_0.jpeg)

![](_page_18_Figure_2.jpeg)

![](_page_19_Picture_0.jpeg)

# LES is by construction a temporally dependent CFD solution:

By construction large scale transient flow phenomena issued by LES will be representative of the physics controlling this single flow realization, i.e.:

1/ set of BC's and IC's

2/ careful with the modeling (loss of causality

and locality at the sub-grid and nearby scales...)

![](_page_19_Figure_7.jpeg)

![](_page_20_Picture_0.jpeg)

#### II.2 ] Transient reacting flows: ignition process understanding

In the initial phase following the energy deposit:

=> Change in slope of the fuel consumption rates

=> Failed case: most of the flame heat is used to evaporate the surrounding liquid fuel until a sudden drop.

=> **Successful case**: slow evolution of the mass transfer rate.

=> Major differences in the local values of the gaseous fuel mass fraction:

- ous fuel mass fraction: - Failed case: too rich to fully evaporate the liquid fuel crossing the flame kernel
- **Successful case**: local variations at the flame kernel position ensure full ignition

![](_page_20_Figure_9.jpeg)

![](_page_21_Picture_0.jpeg)

For modeling and understanding you need different realizations of the ignition sequence:

=> use of statistically stationary cold LES and start the energy deposit at different instants

![](_page_21_Figure_4.jpeg)

#### Outline of the talk

![](_page_22_Picture_1.jpeg)

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![](_page_22_Picture_14.jpeg)

Radial position [%]

![](_page_22_Figure_15.jpeg)

![](_page_22_Picture_16.jpeg)

![](_page_22_Picture_17.jpeg)

![](_page_22_Picture_18.jpeg)

![](_page_23_Picture_0.jpeg)

Engine design: increase the engine efficiency, reduce fuel consumption and pollutant emissions

#### - Efficiency:

![](_page_23_Figure_4.jpeg)

![](_page_23_Picture_5.jpeg)

- Low NOx design: increase the amount of air going through the fuel injection system to increase premixing and lean combustion
  - => highly prone to combustion thermo acoustic instabilities
  - => less 'fresh' air to dilute the hot gases entering the turbine...

![](_page_23_Picture_9.jpeg)

![](_page_24_Picture_0.jpeg)

#### LES imposes constraints:

#### Natural pre-requisites:

=> Interfacing massively parallel codes while preserving their respective scalability

=> Preserve the overall CPU cost of the new massively parallel application

#### Co-lateral scientific issues:

=> non-coincident meshes, interpolations schemes, numerical stability...

![](_page_24_Figure_8.jpeg)

![](_page_25_Picture_0.jpeg)

#### Aerothermal coupling simulations

- T120D configuration (VKI),
- AVBP/AVTP coupling simulation [1],
- Mesh is 6,5 millions of cells.

- Outlet Mach number: 0.87,
- Re = 4.0 10<sup>5</sup>,
- scheme: TTGC (3rd order),
- WALE turbulence model.

![](_page_25_Figure_10.jpeg)

![](_page_26_Picture_0.jpeg)

#### Outline of the talk

![](_page_27_Picture_1.jpeg)

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![](_page_27_Picture_14.jpeg)

1.5 2.0 time after t0 [s]

28

1.0

![](_page_27_Picture_15.jpeg)

![](_page_28_Picture_0.jpeg)

#### **III** ] Conclusions and Perspectives

#### LES of industrial burners:

=> intermediate resolution and simple models seem sufficient

=> difficulties are in the cooling system modeling and introduced

to be able to produce de computations (careful!!)

=> brute force LES is also possible but costly

#### LES perspectives and applications:

- => LES modeling and code validations is still needed: two-phase flows!!
- => Transient reacting flows: ignition process understanding
- => Towards multi-physics CFD based on LES

![](_page_28_Picture_11.jpeg)

![](_page_28_Picture_12.jpeg)

![](_page_28_Figure_13.jpeg)

![](_page_28_Figure_14.jpeg)

![](_page_28_Picture_15.jpeg)

EFF/CS

![](_page_29_Picture_0.jpeg)

#### **Thanks for your attention**

Any questions?

![](_page_29_Figure_3.jpeg)

#### Thanks to the CERFACS-CFD team and our partners!

http://www.cerfacs.fr/~lgicquel Laurent.Gicquel@cerfacs.fr

![](_page_29_Picture_6.jpeg)

![](_page_30_Picture_0.jpeg)

B. Franzelli et al., C&F, 157:1364-1373, 2010.
 W.P. Jones et al., C&F 73:222-233, 1988.
 N. Peters, Vol. 241, Springer, Berlin, 1985.

# Instantaneous CH4 oxidation and CO-CO2 recombination

![](_page_30_Figure_4.jpeg)

![](_page_30_Picture_5.jpeg)

#### **CERFACS** CFD – Combustion Group

![](_page_31_Picture_1.jpeg)

# The aeronautic context

- CO<sub>2</sub> emissions from 1990 to 2025<sup>1</sup>: +100-600% (2008: 2.2% of the total).
- European objectives for 2020<sup>2</sup>:
  - ➤ reduce pollutant emissions
  - (NO<sub>x</sub>: -80%, CO<sub>2</sub>: -50%),
  - $\succ$  reduce the noise emissions (-10dB).
- Economical constraints:
  - ➤ cut the engine costs (today it represents 30% of the aircraft cost).

![](_page_31_Picture_10.jpeg)

![](_page_31_Picture_11.jpeg)

[1] INRETS, 2004[2] ACARE recommendations

Economical and environmental constraints impose technical and technological changes!

![](_page_31_Picture_14.jpeg)

![](_page_32_Picture_0.jpeg)

**Parallel implementation** 

**Communication strategy: MPI non-blocking calls** 

How to compute a residual at partition interfaces?

![](_page_32_Figure_4.jpeg)

Like this...

![](_page_33_Picture_0.jpeg)

#### Impact of rounding errors on LES

Consequence of the lack of associativity property (Floating point arithmetic):

> illustration on a temporally evolving turbulent channel (AVBP).

![](_page_33_Figure_5.jpeg)

![](_page_33_Picture_6.jpeg)

Senoner et al., 2008

![](_page_34_Picture_0.jpeg)

#### **Impact on numerical solutions**

#### Impact of rounding errors on LES

![](_page_34_Figure_3.jpeg)

![](_page_35_Picture_1.jpeg)

#### Impact of mesh-partitioning

- Non-blocking communications participate to rounding errors (non-deterministic behavior),
- Blocking communications are good for deterministic behavior,
- Any sufficiently turbulent flow computed in LES exhibits significant sensitivity to small perturbations, leading to instantaneous solutions which can be totally different,
- The divergence of solutions is explained by 2 combined factors:
  - > exponential separation of trajectories in turbulent flows,

> propagation of rounding errors induced by domain partitioning and scheduling operations that can be different.

• Implicit stages done on a block basis can result in different convergence/instantaneous solutions:

➢ in practice, this also impacts RANS convergence history... However since the solution is unique (?) and stationnary there should be no degradation of solution observed.

Validation of LES code after modifications may only be based on statistical fields!

![](_page_35_Picture_12.jpeg)

![](_page_36_Picture_1.jpeg)

- 1 Introduction
  - Context
- **2** Numerical developments for HPC
  - Flow solver examples
  - Speed-up and Mesh-partitioning
  - Communication, Impact on numerical solutions

# 3 Application to aeronautic challenges

- Civil aircrafts
- Compressor
- Combustion chambers
- Turbines
- 4 Conclusion and perspectives

![](_page_36_Figure_14.jpeg)

![](_page_36_Picture_15.jpeg)

![](_page_36_Picture_16.jpeg)

![](_page_36_Picture_17.jpeg)

![](_page_36_Picture_18.jpeg)

#### **Turbines**

![](_page_37_Picture_1.jpeg)

#### **Objectives**

- As for compressors, unsteady flows are still not well understood,
- Main reasons are also computational cost, size and complexity of the configurations,
- Challenges today for turbine designers is the prediction of heat transfer:
  - a 15 K difference on the temperature prediction leads to a reduction of its life duration by a factor 2,
  - $\succ$  (U)RANS methods are not adapted to complex flows.

![](_page_37_Picture_8.jpeg)

![](_page_37_Picture_9.jpeg)

![](_page_38_Picture_0.jpeg)

![](_page_38_Picture_1.jpeg)

#### Aerothermal in turbine blades: overview

![](_page_38_Figure_3.jpeg)

Complex flows that can not be efficiently computed with a (U)RANS method:

- laminar to turbulent transition,
- hot spot incoming from the combustion chamber,
- aero-thermal interactions (adiabatic is not true).

![](_page_38_Figure_8.jpeg)

![](_page_38_Figure_9.jpeg)

![](_page_38_Picture_10.jpeg)

![](_page_39_Picture_0.jpeg)

0.05

0.03

0.02

0.01

0.05

0.04 0.03 0.02 0.01 0

Ō

CERF/CS

#### Impact on unsteady aerodynamic performance

![](_page_39_Figure_2.jpeg)

T. Léonard et al., in ASME Turbo-Expo, Glasgow, 2010.

**Turbines** 

![](_page_39_Figure_4.jpeg)

- URANS predicts the vortex shedding but flow features are damped by artificial viscosity,
- LES demonstrates its capacity to transport flow vortices and acoustic waves.

![](_page_39_Picture_7.jpeg)

![](_page_40_Picture_0.jpeg)

CFD research in Turbulent Reacting Flows has massively transitioned LES:

- the continuous increase of computing power
- code developments to ensure scalability of the solvers

![](_page_40_Picture_5.jpeg)

![](_page_41_Picture_0.jpeg)

# I.1 ] Massively parallel context – brief overview of 2000-2010

**AVBP** 

# AVBP: An unstructured LES flow solver:

- Developed by CERFACS and IFP-EN,
- External/internal flows,
- Fully compressible turbulent reacting flows,
- DNS/LES approaches,
- Unstructured hexaedral, tetraedral, prisms & hybrid meshes,
- Massively parallel,
- C/Fortran languages,
- SPMD approach.
- Multi-phase solvers (Lagrangian & Eulerian)

![](_page_41_Figure_12.jpeg)

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![](_page_41_Figure_14.jpeg)

Unstructured grid

(Coincident interfaces)

![](_page_41_Picture_17.jpeg)

![](_page_42_Picture_0.jpeg)

Gaseous turbulent combustion validation:

Two-phase flow combustion

MERCATO burner [1,3]: atmospheric rig targeted to understand two-phase flow combustion --> Measured profiles of Velocity (PIV), Droplet particle size & velocity in cold/reactg cdts

![](_page_42_Picture_5.jpeg)

R. Lecourt et al, .
 M. Sanjose et al.
 M. Sanjose et al, CTR, 2007.

![](_page_42_Figure_7.jpeg)

![](_page_42_Figure_8.jpeg)

![](_page_42_Figure_9.jpeg)

![](_page_43_Picture_0.jpeg)

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#### I.2 ] LES modeling and code validations

![](_page_43_Figure_2.jpeg)

![](_page_44_Picture_0.jpeg)

#### I.2 ] LES modeling and code validations

#### Two-phase reacting flow predictions

![](_page_44_Picture_3.jpeg)

#### **Droplet mass fraction**

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![](_page_44_Figure_5.jpeg)

# Time = 0.400000 Phi 3.50 2.62 1.75 0.88 0.00

Gas equivalence ration

![](_page_45_Picture_0.jpeg)

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#### I.2 ] LES modeling and code validations

#### Two-phase reacting flow predictions

![](_page_45_Figure_3.jpeg)

# I.3] Real scale applications

However and if mastered, it can be fast and make the difference for burner designs (or at least *improve our understanding of real flow applications*)

Feed back / Complexity

J. Schlüter et al, I.J.CFD, 18(3):235-246, 2004.
 L. Selle et al, C&F, 145(1-2):194-205, 2006.
 G. Boudier et al, C&F, 155:196-214, 2008.
 M. Boileau et al., C&F, 154(1-2):2-22, 2008.
 G. Staffelbach et al., 32<sup>nd</sup> Symp., 2008.
 E. Riber et al, JCP, 228(2):539-564, 2009.
 F. Jaeqle, PhD dissertation, INPT, 2009.

[2]

![](_page_46_Picture_4.jpeg)

Resources required for an LES

200

[1]

#### Outline of the talk

![](_page_47_Picture_1.jpeg)

I] Recent contributions of LES to Combustor design:

- => Massively parallel context brief overview of 2000-2010
- => LES modeling and code validations
- => Real scale applications
  - -> comparison against RANS predictions
  - -> thermo-acoustic instability prediction

# II ] LES perspectives and applications:

=> Transient reacting flows: ignition process understanding

(0)

=> Towards multi-physics CFD based on LES

III ] Conclusions and Perspectives

![](_page_47_Picture_13.jpeg)

![](_page_47_Picture_14.jpeg)

Radial position [%]

Ignition tests with  $E_{deo}$ =100mJ and  $\Delta t_{deo}$ =50 $\mu$ s

1.0 1.5 2.0

time after t0 [s]

2.5 3.0x10<sup>-3</sup>

![](_page_47_Picture_15.jpeg)

![](_page_47_Picture_16.jpeg)

![](_page_48_Picture_0.jpeg)

Improving the temperature field predictions in the burners:

![](_page_48_Picture_3.jpeg)